



**Науковий вісник Львівського національного університету  
ветеринарної медицини та біотехнологій імені С.З. Гжицького.  
Серія: Харчові технології**

**Scientific Messenger of Lviv National University  
of Veterinary Medicine and Biotechnologies.  
Series: Food Technologies**

ISSN 2519-268X print  
ISSN 2707-5885 online

doi: 10.32718/nvlvet-f9701  
<https://nvlvet.com.ua/index.php/food>

UDC 539.23

## **Production of thin film of multicomponent inorganic semiconductors under quasi-equilibrium conditions**

B. Tsizh<sup>1,2✉</sup>, Z. Dziamski<sup>1</sup>

<sup>1</sup>Kazimierz Wielki University in Bydgoszcz, Bydgoszcz, Poland

<sup>2</sup>Stepan Gzhytskyi National University of Veterinary Medicine and Biotechnologies Lviv, Lviv, Ukraine

### *Article info*

Received 17.01.2022

Received in revised form

17.02.2022

Accepted 18.02.2022

Kazimierz Wielki University in  
Bydgoszcz, 30 Chodkiewicza,  
Bydgoszcz, 85-064, Poland.

Stepan Gzhytskyi National  
University of Veterinary Medicine  
and Biotechnologies Lviv,  
Pekarska Str., 50, Lviv,  
79010, Ukraine.  
Tel.: +38-032-239-26-35  
E-mail: tsizhb@ukr.net

**Tsizh, B., & Dziamski, Z. (2022). Production of thin film of multicomponent inorganic semiconductors under quasi-equilibrium conditions. Scientific Messenger of Lviv National University of Veterinary Medicine and Biotechnologies. Series: Food Technologies, 24(97), 3–8. doi: 10.32718/nvlvet-f9701**

Issues of improving the properties of semiconductor thin film and their reproducibility, as well as improving and reducing the cost of manufacturing technology stimulate research and development of new, advanced methods. Therefore, it is important to optimize the technology of getting reproducible, competitive, high-tech thin films of multicomponent semiconductor compounds with predetermined properties. In the given article it is shown that constructive and technological improvements of a method of thermal spraying in vacuum allow to minimize nonequilibrium conditions of film growth, keeping the advantages of thermovacuum spraying, such as high reproducibility, processability and productivity, a wide range of variations in the synthesis conditions, and, accordingly, the properties of condensates, maximum purity of growth processes, as well as ease of performing and management and cost-effectiveness of the process of getting perfect condensates. For this purpose, we have developed a special construction of a quasi-fusion evaporator and a device for getting semiconductor film in vacuum, as well as a version of a transparent "hot wall". The resistivity, cross section and geometric dimensions of the cover and the heater of the developed structures were selected so that in the mode of resistive heating of the evaporator temperature gradient due to the difference in their electrical resistance, and, accordingly, the Joule heat of current, in the temperature range 673... 1473 K provided the temperature of the cover 1.1 ... 1.3 times higher than the temperature of the heater. Due to the elevated temperature of the cover, the solid fraction is either repelled on the sublimating (evaporating) surface and the walls of the crucible, or undergoes sublimation (evaporation) from the surface of the cover. Depending on the values of the sputtering rate, the grain size of semiconductor polycrystalline film varied from units of nanometers to several micrometers. Crystallinely ordered films were got at relatively low values of the sputtering rate (0.5...5 nm·s<sup>-1</sup>). It was set up the technological conditions for getting thin films of multicomponent semiconductors, which ensure the independence of the chemical composition of condensates from the evaporation rate in the wide range from 0.05 to 20 nm·s<sup>-1</sup>, uniform composition of the gas phase during sublimation, absence of inhomogeneous solids in films, wide range properties of condensates and their high reproducibility.

**Key words:** thin films, semiconductors, technological methods of obtaining, thermal spraying, quasi-equilibrium conditions.

## **Отримання тонких плівок багатокomпонентних неорганічних напівпровідників у квазірівноважних умовах**

Б. Ціж<sup>1,2✉</sup>, З. Дзіамські<sup>1</sup>

<sup>1</sup>Kazimierz Wielki University in Bydgoszcz, Bydgoszcz, Poland

<sup>2</sup>Львівський національний університет ветеринарної медицини та біотехнологій імені С. З. Гжицького, м. Львів, Україна

*Питання поліпшення властивостей напівпровідникових тонких плівок і їхньої відтворюваності, а також удосконалення і зде- шевлення технології їх виготовлення стимулюють дослідження і розробку нових, прогресивних методик. Тому важливою є оптимізація технології отримання відтворюваних, конкурентоздатних, високотехнологічних тонких плівок багатокомпонентних напівпровідникових сполук із наперед заданими властивостями. В даній статті показано, що конструктивні та технологічні вдосконалення методу термічного наплення у вакуумі дозволяють мінімізувати нерівноважні умови росту плівок, зберігаючи при цьому такі переваги термовакуумного наплення, як високі відтворюваність, технологічність і продуктивність, широкий спектр варіювання умовами синтезу, а відповідно і властивостями конденсатів, максимальна чистота процесів росту, а також простота виконання і керування та економічність процесу отримання досконалих конденсатів. Для цього нами розроблена спеціальна конструкція квазіефузійного випарника та пристрій для отримання напівпровідникових плівок у вакуумі, а також варіант прозорі "гарячої стінки". Питомий опір, поперечний переріз і геометричні розміри кришки і нагрівника розроблених конструкцій підбирали таким чином, щоби в режимі резистивного нагрівання випарника градієнт температур за рахунок різниці їх електроопору, а відповідно і Джоулевої теплоти струму, в температурному інтервалі 673...1473 К забезпечував температуру кришки в 1,1...1,3 раза більшу від температури нагрівника. За рахунок підвищеної температури кришки твердотільна фракція або відштовхується на сублимуючу (випаровуючу) поверхню і стінки тигля, або зазнає сублимації (випаровування) з поверхні кришки. Залежно від значень швидкості наплення розмір зерен напівпровідникових полікристалічних плівок змінювався від одиниць нанометрів до декількох мікрометрів. Кристалічно впорядкованіші плівки отримували при порівняно низьких значеннях швидкості наплення (0,5...5 нм·с<sup>-1</sup>). Встановлено технологічні умови отримання тонких плівок багатокомпонентних напівпровідників, які забезпечують незалежність хімічного складу конденсатів від швидкості випаровування в широких межах від 0,05 до 20 нм·с<sup>-1</sup>, рівномірний склад газової фази при сублимації, відсутність неоднорідних твердотільних включень у плівках, широкий спектр фізичних властивостей конденсатів та їхню високу відтворюваність.*

**Ключові слова:** тонкі плівки, напівпровідники, технологічні методи отримання, термічне наплення, квазірівноважні умови.

## Introduction

In previous reviews (Tsizh & Dziamski, 2019; 2020) we have given an analysis of existing methods for applying thin films of inorganic semiconductor materials. This analysis showed that the technological aspects of obtaining semiconductor films have been studied in detail for many years and today we have formed dozens of relevant methods and technological regulations. However, the issues of improving the properties of semiconductor films and their reproducibility, as well as improving and reducing the cost of production technology stimulate research and development of new, advanced techniques (Bunshah, 1994; Seshan, 2002; Hosokawa et al., 2008; Bahmut, 2014; Hartmut & Hamid, 2015; Antoniuk, 2016; Shahini-an, 2017). Therefore, a significant amount of our research was devoted to the optimization of the technology of reproducible, competitive, high-tech thin films of multicomponent semiconductor compounds with predetermined properties (Aksimentyeva et al., 2018).

The choice of method of manufacturing thin films is determined by the optimal expected set of their properties in combination with the maximum reproducibility, manufacturability and economy of the process. After analyzing the known methods of obtaining semiconductor condensates, we focused in more detail on thermal spraying in vacuum, which, despite the nonequilibrium conditions of films growth, has good manufacturability, a wide range of variations in synthesis conditions, and, accordingly, the properties of condensates, maximum purity of growth processes, reproducibility, productivity, as well as ease of execution and management, which makes it a universal method for many modern developments, in particular, for the creation of thin-film sensitive elements for gas sensors and other electronic devices, including for use in the food and processing industries. In addition, the results of constructive and technological improvements in the method of thermal spraying in vacuum give reason to hope to minimize the imbalance of the conditions of film growth and obtaining perfect condensates.

## Material and methods

The application of multicomponent semiconductor thin films of materials such as compounds  $A_3B_5$ ,  $A_2B_6$ , chalcogenide glassy semiconductors, oxides and others was carried out in serial installations of vacuum spraying as previous generations, such as YPM 3.279.011 with high-oil high-vacuum pump and YPM 3.279.047 with high-vacuum ion-getter pump, and in the modern combined installation of vacuum spraying of thin films produced by "Torr International" (USA). Glass, quartz, sileand other plates were used for substrates. The substrates were heated by infrared radiation of quartz lamps, the temperature was controlled by chromel-aluminum thermocouples.

To improve the quality and adhesion of condensates, chemical and, in some cases, ionization cleaning of substrates was performed before spraying. Technology was used and allows to quickly and efficiently remove contaminants, including organic in nature. The glass substrates, after pre-degreasing with acetone, were cleaned by boiling in hydrogen peroxide solution in the presence of ammonia, followed by washing in hot deionized water and drying in isopropyl alcohol vapor. Ultrasonic excitation was used for more effective action of detergents. In addition, before spraying, the substrates were heat-cleaned in vacuum by half-hour heating at 623 K.

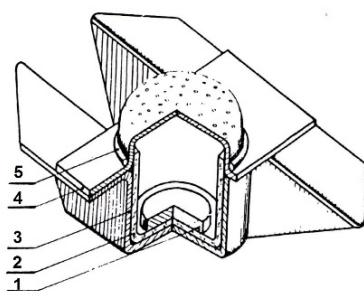
The control of the sputtering speed and the thickness of the films during their growth was performed by the optical method, which is based on the interference of transmitted light beams, due to reflection from the boundaries of the films with the substrate and vacuum. In this case, the increase in the physical thickness of the films by a value equal to a quarter of the wavelength  $\lambda$  of light, corresponds to an increase in the order of the interference extremum. Since in the field of film transparency the value of the refractive index weakly depends on  $\lambda$ , the interference pattern was isolated using an interference filter with a bandwidth of  $\lambda = 774 \pm 15$  nm, which increases the accuracy of measurements. In addition, in the field of films transparency there are no undesirable processes of reducing the intensity of the interference pattern

due to absorption. In the installations used by us blocks of optical control are provided, that allow modulation, isolation and amplification of the useful light signal, which provided the measurement of condensate thickness with an accuracy of at least 10 nm at the extremes and 20 nm between them.

In addition to controlling the thickness of the films in the spraying process, thickness measurements were performed on an МІІІ-4 interference microscope and on two-beam spectrometers. Microinterferometer of Linnik МІІІ-4 made it possible to measure the height of irregularities of thin films, such as etched edge, scratches and others from 0.1 to 5  $\mu\text{m}$  with an accuracy of 6 % by using the phenomenon of interference reflected from the surface of the films and substrate, pre-separated light beams, coming from one point of the source. To increase the measurement accuracy, the films thickness with  $d < 0.5 \mu\text{m}$  was determined in parallel from the values of the difference in optical densities  $D - D_0$ . To do this, the wavelength at which  $0.5 < D < 2.0$  for films of this composition with  $0.1 < d < 0.5 \mu\text{m}$  was chosen on the spectral dependence  $D$ , and the value of  $d$  was specified according to the calibrated dependence  $D(d)$ . This allowed to increase the accuracy of measuring the thickness of the films up to 4 % in the thickness range of 0.1 ... 0.5  $\mu\text{m}$ .

## Results and discussions

Due to the disadvantages of the existing evaporators, we have developed a special design of the quasi-fusion evaporator and a device for obtaining semiconductor films in vacuum, schematically shown in Fig. 1 and 2, respectively, as well as a variant of a transparent "hot wall" (Fig. 3) (Aksimentyeva et al., 2018). The thermal quasi-fusion evaporator for vacuum spraying (Fig. 1) consists of a cylindrical quartz crucible (2) with a height of 25 ... 35 mm, a diameter of 15 ... 25 mm and a wall thickness of 1 ... 1.5 mm, which, together with the tablet (1) of the source semiconductor material, is placed in a tantalum or molybdenum heater (3), that provides uniform heating, and tightly, with a clamp (5), close the tantalum or molybdenum lid with 40 ... 60 holes with a diameter of 0.1 ... 0.3 mm, adapted to pass current through it.

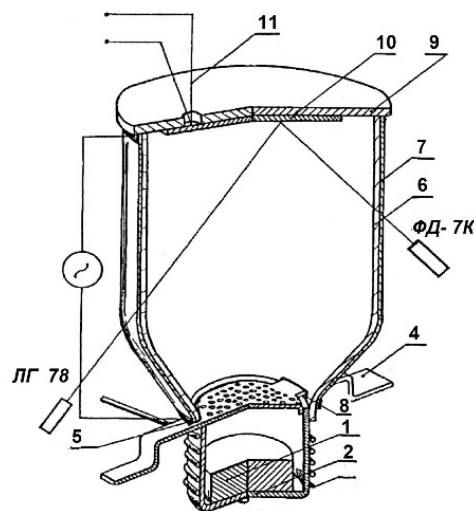


**Fig. 1.** The design of a thermal quasi-fusion evaporator for spraying semiconductor thin films in vacuum:

- 1 – tablet of source material, 2 – quartz crucible,
- 3 – tape heater, 4 – perforated lid, 5 – sealing clamp

The device for obtaining semiconductor films in vacuum (Fig. 2) consists of a quartz chamber (6) 130 mm high with a wall thickness of 2 mm, made in the form of a

cylinder that smoothly transitions into an inverted truncated cone, upper and lower outer diameters of 70 and 25 mm, with slots (8) under the cover (4).

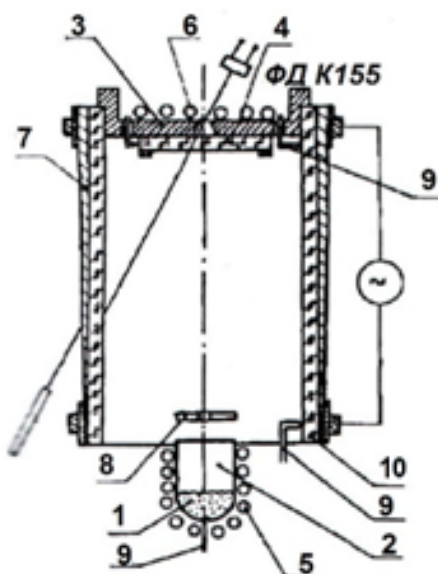


**Fig. 2.** Device for obtaining semiconductor films in vacuum: 1 – tablet of starting material, 2 – quartz crucible, 3 – evaporator heater, 4 – perforated evaporator cover, 5 – conductive tires, 6 – quartz evaporation chamber, 7 – transparent resistive heater, 8 – slots on the cover, 9 – substrate holder, 10 – substrate, 11 – thermocouple

A thin ( $\sim 0.2 \mu\text{m}$ ) layer of a mixture of oxides of indium and stannum (7) with optical transmission  $T = 97\%$  ( $\lambda = 633 \text{ nm}$ ) was applied to the outer walls of the chamber by high-frequency ion-plasma sputtering of the target ( $\text{In}_2\text{O}_3$ ) 90 ( $\text{SnO}_2$ ) 10 in vacuum and the specific electrical surface resistance  $\rho_{\text{II}} = 300 \text{ Ohm} \cdot \text{cm}^{-2}$ . At both ends of the chamber alternate thermal spraying in a vacuum of Cr-Cu-Ni films with a total thickness of about 2  $\mu\text{m}$  and a width of 5 mm electrically conductive busbars (5) are applied for uniform current flow through the heater. In a cylindrical quartz evaporator (2) with a height of 30 mm and a diameter of 20 mm with a wall thickness of 1.5 mm load a tablet (1) of starting material. The evaporator is inserted into a tantalum, molybdenum or tungsten heater (3), which ensures uniform heating, and tightly closed with a tantalum lid (4) with fifty holes with a diameter of 0.2 ... 0.4 mm. The evaporation chamber is placed on the evaporator and the tires, the evaporator heater and the cover are connected to the heat source. A stainless steeldisc holder (9) is placed on the chamber and a substrate (10) and a thermocouple (11) are attached to it. The substrate is heated by infrared radiation of quartz lamps. He-Ne laser ЛГ-278 and photodiode ФД-7К are used for optical control of film thickness. Tablets of the starting material were compressed from a mechanical mixture of the required ratio of fine dispersed powders of the selected semiconductors. In both cases, the crucible heater and the lid were connected to a common source of electric heat.

Similar structural elements are present in the device, which is commonly called the "hot wall" (Fig. 3).





**Fig. 3.** Construction of a “hot wall” for thermal spraying of semiconductor thin films in a quasi-closed volume: 1 – source material, 2 – evaporator, 3 – substrate holder, 4 – substrate, 5 – evaporator heater, 6 – substrate heater, 7 – wall heater, 8 – reflective screen, 9 – thermal steam, 10 – quartz cylinder

This device does not have a crucible lid, and the problem of preventing direct contact of the subliming material on the substrate is solved using a protective reflective screen (Fig. 3, 8). In addition, there is no tight contact between the crucible (evaporator) 2 and the quartz cylinder 10, which makes the process of condensate synthesis less balanced, but simplifies the construction and makes this type of thermovacuum spraying more widely available.

The resistivity, cross section and geometric dimensions of the cover and the heater in the first and second versions (Fig. 1 and 2) were selected so that in the mode of resistive heating of the evaporator temperature gradient due to the difference in their electrical resistance, and, accordingly, the Joule heat of the current, in the temperature range 673... 1473 K provided the temperature of the cover of the  $T_c$  in 1.1 ... 1.3 times higher than the temperature of the heater  $T_h$ . Such an evaporator can be considered as one of the variants of the Knudsen cell, the mechanism of evaporation of which has its own laws (Kalinkin et al., 1978).

Due to the increased temperature of the lid, the solid fraction is either repelled on the sublimating (evaporating) surface and the walls of the crucible, or undergoes sublimation (evaporation) from the surface of the lid. It is known (Kalinkin et al., 1978) that the diffusion rate from the Knudsen cell is largely determined by the temperature of the lid grows with its increase. Therefore, the vapor pressure of subliming (evaporating) substances in the crucible with increasing  $T_c/T_h$  ratio increases and becomes closer to the saturated vapor pressure compared to the evaporator, in which the lid and the heater have the same temperature. This reduces the difference between the gas pressures of the individual components, which further improves the stoichiometry of semiconductor condensates. In addition, due to the specified temperature

gradient along the vertical axis of the evaporator increases the variable interaction between the vapor and the source material, which improves the homogeneity composition of the gas phase. At the same temperatures of the lid and the heater there is a significant increase in the individual components on the inner side of the lid and their departure from the crucible is due to re-evaporation from the lid. This significantly slows down the spraying process, uncontrollably changes the composition of the vapor phase, and also causes the cover holes to stick. The speed of sublimation in this situation is reduced also because the electrical resistance of the cover decreases due to the condensation of semiconductors on it, while reducing the heat of the Joule, which heats it. In a situation where  $T_c > T_h$  at least 1.1 times the condensation of vapors on the inner surface of the cover is practically absent, semiconductor atoms fly out of its holes without the above-described double sublimation or re-evaporation, spraying can be carried out at temperatures lower than  $T_c = T_h$ . It is convenient to enter some coefficient  $S = T_c/T_h$  as the effective capacity of the evaporator. Then the required temperature gradient of the cover and heater, determined by us empirically for semiconductors of group A<sup>II</sup>B<sup>IV</sup>, can be written as:

$$1.1 < S < 1.3 \text{ at } 600 \text{ K} < T_h < 1400 \text{ K.} \quad (1)$$

The temperature limits of condition (1) are due to experimental data that at values of  $T_h < 600$  K the sublimation process is very slow, with a significant (> 1 atomic %) deviation from the stoichiometry, and at  $T_h > 1400$  K high temperatures of the heater material and, especially, the lids contribute to its rapid (after 2–3 loads of the crucible) burnout, which is accelerated by the corrosive action of semiconductor components at high temperatures.

From the dependences of the values of  $S$  on the degree of filling of the evaporator crucible with the starting material, we determined that when the crucible is filled by 30–70 % there is a certain stabilization of the temperature gradient of the lid and heater. Therefore, the first and last phases of spraying, as less stable and non-congruent, were performed using a damper.

The evaporators developed by us allowed to create molecular fluxes of vapors of subliming compounds of regulated intensity homogeneous in composition in a wide range of application conditions, which made it possible to get homogeneous, reproducible films of stoichiometric composition at different spray rates. In the case of using evaporators with non-compliance with ratio (1), the quality of the films deteriorated sharply: welded protrusions appeared due to the sedimentation of the solid fraction of steam, for the same concentration of the source material, the chemical composition of the film significantly depended on the spray rate, there was often a strong deviation from the stoichiometric composition (up to 5 ... 7 atomic %), deteriorating the homogeneity of the films in area and reproducibility of their properties, evaporation was accompanied by undesirable processes of sticking holes in the evaporator cover, which prevented the gas phase.

The described thermal evaporators have the following advantages over the known closed-type evaporators used for spraying thin films of semiconductor compounds:

- independence of the chemical composition of condensates from the evaporation rate in a wide range from  $0.05$  to  $20 \text{ nm} \cdot \text{s}^{-1}$ ;
- uniform composition of the gas phase during sublimation;
- absence of inhomogeneous solid inclusions in the films;
- no sticking processes of the lid outlets.

In addition, in the device with a heating chamber (Fig. 2) tight connection of the evaporation chamber with the evaporator brings this construction closer to a quasi-closed volume, in this case, in contrast to the latter, it is possible to optically control the thickness of the films and their growth rate.

One of the most important technological parameters in the thermal spraying of semiconductor thin films in vacuum is the lining temperature ( $T_l$ ) and the spray rate ( $V_h$ ).  $T_l$  influences on the ratio of components that condense and re-evaporate. Continuous predominant vapor condensation of this substance is possible only for temperatures lower than critical.

With the growth of  $T_l$  the migration of sublimated molecules is increasing on the condensation surface, while the association of molecules of individual components improves, and although the reflection of their vapors also increases, the process of formation of homogeneous, stoichiometric condensates stabilizes.  $V_h$  spray rate has an influence on the structure and properties of semiconductor films. Due to the processes of re-evaporation and desorption from the substrate,  $V_h$  condensate is determined by the ratio of  $T_l$  and the rate of vapor flow to the substrate, which in turn depends on the temperature of the evaporator. Depending on the  $V_h$  values, the grain size of semiconductor polycrystalline films can vary from nanometer units to several micrometers. Crystallinely more ordered films were got at relatively low  $V_h$  values ( $0.5 \dots 5 \text{ nm} \cdot \text{s}^{-1}$ ).  $V_h$  has also an influence on the composition of the films. For small ( $0.05 \dots 0.2 \text{ nm} \cdot \text{s}^{-1}$ ) and large ( $30 \dots 50 \text{ nm} \cdot \text{s}^{-1}$ )  $V_h$  values, deviations of the molar ratio of semiconductor components from stoichiometric to a few percent were observed. In most works, the optimal  $V_h$  of semiconductor layers is in the range from a few tenths to several units of  $\text{nm} \cdot \text{s}^{-1}$ .

In addition to the values of  $T_l$  and  $V_h$ , the depth of vacuum and the composition of residual gases in the spraying process have a significant influence on the structural features and properties of semiconductor condensates. In order to effectively control the growth processes and good reproducibility of the properties of thin films, it is necessary to ensure the cleanest possible conditions of preparation. This is achieved by improving the vacuum, increasing the purity of the source components, minimizing the influence of the evaporator material on the properties of the films.

## Conclusions

This article shows that the construction and technological improvements of the method of thermal spraying in

vacuum can minimize the nonequilibrium conditions of film growth, while maintaining the following advantages of thermovacuum spraying, such as high reproducibility, processability and productivity, a wide range of variations in the conditions of synthesis, and, accordingly, the properties of condensates, maximum purity of growth processes, as well as ease of execution and management and cost-effectiveness of the process of getting perfect condensates. Technological conditions for getting thin films of multicomponent semiconductors, which ensure the independence of the chemical composition of condensates from the evaporation rate in a wide range from  $0.05$  to  $20 \text{ nm} \cdot \text{s}^{-1}$ , uniform composition of the gas phase during sublimation, the absence of inhomogeneous solid inclusions in the films, a wide range of physical properties of condensates and their high reproducibility.

**Perspectives for further research.** Further research should continue to optimize the methods of getting thin films of multicomponent inorganic semiconductors in order to achieve the highest degree of equilibrium conditions of condensate growth and, consequently, to improve their properties. To do this, it is necessary to develop new constructions of devices for the synthesis of thin films and improve the technological regulations for their receipt.

## Acknowledgments

This work was supported by the project of Ministry of Education and Science of Ukraine "Development of composite organo-inorganic heterostructures for reversible gas sensors" (state registration number 0120U101998).

## Conflict of interest

The authors state that there is no conflict of interest.

## References

- Aksimentyeva, O., Tsizh, B., & Chokhan', M. (2018). Sensory kontrolyu gazovyh seredovyshch u harchoviy promyslovosti ta dovkilli: monografiya. Lviv, Piramida (in Ukrainian).
- Antoniuk, V. S., Tymchyk, G. S., Bondarenko, Yu. Yu., Kovalenko, Yu. I., Bondarenko, M. O., & Gaydash, R. P. (2016). Pokryttia u pryladobuduvanni. Kyiv, Politehnika. URL: <http://ena.lp.edu.ua:8080/handle/ntb/36387> (in Ukrainian).
- Bahmut, A. H. (2014). Elektronnaya mikroskopiya plyonok, osazhdiennykh lazernym isparieniyem: monografiya. Harkiv, NTU "HPI". URL: [http://repository.kpi.kharkov.ua/bitstream/KhPI-Press/10107/1/Bagmut\\_Elekt\\_r\\_mikroskopiya\\_2014.pdf](http://repository.kpi.kharkov.ua/bitstream/KhPI-Press/10107/1/Bagmut_Elekt_r_mikroskopiya_2014.pdf) (in Russian).
- Hartmut, F., & Hamid, R. K. (2015). Handbook of Thin Film Technology, Springer. URL: <https://www.springer.com/us/book/9783642054297>.
- Bunshah, R. F. (1994). Handbook of Deposition Technologies for Films and Coatings.. New Jersey, Noyes Publication. URL: <https://www.elsevier.com/books/handbook-of-deposition-technologies-for-films-and-coatings/bunshah/978-0-8155-1337-7>.
- Seshan, K. (2002). Handbook of Thin Film Deposition Processes and Techniques. Edited by New York, Noyes Publication / William Andrew Publication.

- URL: <https://www.elsevier.com/books/handbook-of-thin-film-deposition/seshan/978-1-4377-7873-1>.
- Kalinkin, I. P., Alieskovskiy, V. B., & Simashkievich, A. V. (1978). Epitaksial'nyie plionki soyedin ieniy A<sup>II</sup>B<sup>VI</sup>. Leningrad, Izdatielstvo Leningradskogo universiteta (in Russian).
- Hosokawa, M., Naito, M., Nogi, K., & Yokoyama, T. (2008). Nanoparticle Technology Handbook. New York, Elsevier B.V. URL: <https://www.sciencedirect.com/book/9780444531223/nanoparticle-technology-handbook#book-info>.
- Shahinian, L. R. (2017). The Mechanisms of Formation of Thin Films and Coatings Deposited by Physical Vapor Deposition Technology. Kyiv, Akademperiodyka. URL: [http://akademperiodyka.org.ua/en/books/the\\_mechanisms\\_of\\_formation\\_of\\_thin\\_films\\_and\\_coatings\\_deposited\\_by\\_physical\\_vapor\\_deposition\\_technology](http://akademperiodyka.org.ua/en/books/the_mechanisms_of_formation_of_thin_films_and_coatings_deposited_by_physical_vapor_deposition_technology).
- Tsizh, B., & Dziamski Z. (2019). Technological Methods of Forming Thin Semiconductor Layers. Part 1. Scientific Messenger LNUVMB. Series: Food Technologies, 21(91), 20–24. DOI: 10.32718/nvlvet-f9104.
- Tsizh, B., & Dziamski, Z. (2019). Technological Methods of Forming Thin Semiconductor Layers. Part 2. Scientific Messenger LNUVMB. Series: Food Technologies, 21(92), 3–7. DOI: 10.32718/nvlvet-f9201.
- Tsizh, B. & Dziamski, Z. (2020). Technological Methods of Forming Thin Semiconductor Layers. Part 3. Scientific Messenger LNUVMB. Series: Food Technologies, 22(93), 15–17. DOI: 10.32718/nvlvet-f9303.